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UNIVERSITI SAINS MALAYSIA

First Semester Examination  
2012/2013 Academic Session

January 2013

**EKC 336 – Chemical Reaction Engineering**  
***[Kejuruteraan Tindak Balas Kimia]***

Duration : 3 hours  
*[Masa : 3 jam]*

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Please check that this examination paper consists of SIX pages of printed material and SIX pages of Appendix before you begin the examination.

*[Sila pastikan bahawa kertas peperiksaan ini mengandungi ENAM muka surat yang bercetak dan ENAM muka surat Lampiran sebelum anda memulakan peperiksaan ini.]*

**Instruction:** Answer **ALL** (4) questions.

**[Arahan:** Jawab **SEMUA** (4) soalan.]

In the event of any discrepancies, the English version shall be used.

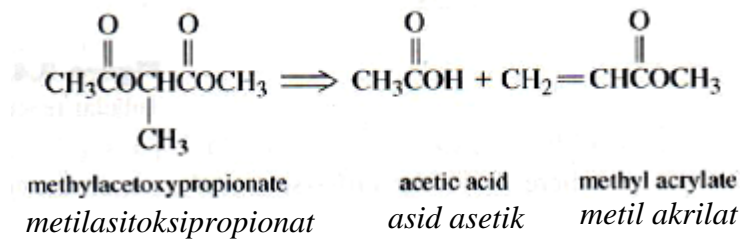
*[Sekiranya terdapat sebarang percanggahan pada soalan peperiksaan, versi Bahasa Inggeris hendaklah diguna pakai.]*

Answer ALL questions.

Jawab SEMUA soalan.

1. [a] A Plug Flow Reactor (PFR) operating isothermally at 773 K is used to conduct the following reaction:

*Sebuah reaktor palam aliran beroperasi secara isoterma pada 773K digunakan untuk menjalankan tindak balas berikut:*



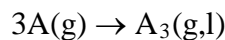
If a feed of pure is the methylacetoxypionate enters at 5 atm and at a flow rate of 20 m<sup>3</sup>/h, what the length of pipe with a cross-sectional area of 0.0036 m<sup>2</sup> is necessary for the reaction to achieve 90 percent conversion?

*Jika suapan tulen metilasetoksipropionat masuk pada 5 atm dan kadar aliran 20 m<sup>3</sup>/j, apakah panjang paip yang mempunyai luas keratan rentas 0.0036 m<sup>2</sup> yang diperlukan bagi tindak balas untuk mencapai penukaran 90 peratus?*

Data:  $k = 7.8 \times 10^9 \exp[-19,200/T], (\text{s}^{-1})$

[10 marks/markah]

- [b] The trimerization  
*Trimerisasi ini*



is carried out isothermally and without pressure drop in a PFR at 298 K and 2 atm. As the concentration of A<sub>3</sub> increases downstream the reactor and A<sub>3</sub> begins to condense. The vapor pressure of A<sub>3</sub> at 298 K is 0.5 atm. If an equal molar mixture of A and inert, (I) is fed into the reactor, at what conversion of A will A<sub>3</sub> begin to condense?

*dijalankan secara isoterma dan tanpa kejatuhan tekanan di dalam sebuah reaktor palam aliran pada 298K dan 2 atm. Kepekatan A<sub>3</sub> meningkat dihilir reaktor dan A<sub>3</sub> mula untuk terpeluwap. Tekanan wap A<sub>3</sub> pada 298K adalah 0.5 atm. Jika campuran molar sama bagi A dan lengai, (I) disuapkan ke dalam reaktor, pada penukaran berapakah A akan bermula memeluwapkan A<sub>3</sub>?*

[8 marks/markah]

- [c] Starting from general mole balance equation, derive the design equation for PFR.

*Bermula dari persamaan umum keseimbangan mol, terbitkan persamaan rekabentuk untuk reaktor palam aliran.*

[7 marks/markah]

2. [a] The decomposition of a halogen was studied, with the results shown in Table Q.2.[a].:

*Penguraian halogen telah dipelajari, dengan keputusan yang ditunjukkan di dalam Jadual S.2.[a].:*

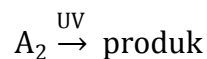
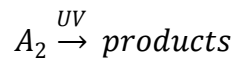


Table Q.2.[a].  
Jadual S.2.[a].

Time (Min) Masa (Min)	C <sub>A</sub> (ppm)
10	2.45
20	1.74
30	1.23
40	0.88
50	0.62
60	0.44

Use the differential method of analysis to determine the rate law, then calculate the required rate of addition (in units of lb/hr) of this halogen necessary to maintain a concentration of 1 ppm in a sun-illuminated, 25,000 gallon pond.

*Gunakan analisis kaedah pembezaan untuk menentukan hukum kadar, kemudian kirakan kadar yang diperlukan untuk penambahan (dalam unit lb/j) bagi keperluan halogen untuk mengekalkan kepekatan 1 ppm di bawah pencahayaan matahari bagi 25,000 gelen kolam.*

(Note: ppm parts of bromine per million parts brominated water by weight. In dilute aqueous solutions, 1 ppm=1 milligram per liter, molecular weight of Br = 80 Daltons.)

*(Nota: bahagian ppm bagi bromin per bahagian juta dibrominkan dengan air berdasarkan berat. Bagi larutan akuas tercair, 1 ppm = 1 miligram per liter, berat molekul Br = 80 Dalton).*

$$1 \text{ gal} \longrightarrow 3.785 \text{ liter}$$

$$1 \text{ lb} \longrightarrow 454 \text{ g}$$

[15 marks/markah]

...4/-

- [b] [i] Prepare a stoichiometric table showing the effluent concentrations of all species of a gas-phase PFR for the stoichiometry  $A \rightarrow B + 2C$ . The reactor feed contains half (molar) inert.

*Sediakan jadual stoikiometri yang menunjukkan kepekatan keluar bagi semua spesis fasa gas reaktor dalam aliran untuk stoikiometri  $A \rightarrow B + 2C$ . Suapan reaktor mengandungi separuh (molar) lengai.*

- [ii] Using the results in the stoichiometric table prepared in Q.2.[b].[i]., define an elementary rate law in terms of conversion.

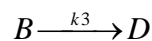
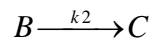
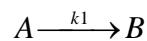
*Gunakan keputusan di dalam jadual stoikiometri yang disediakan dalam S.2.[b].[i]., takrifkan hukum kadar asas berdasarkan penukaran.*

- [iii] By what fraction does  $C_A$  change at 80% conversion?

*Berapakah pecahan bagi  $C_A$  bertukar kepada 80% penukaran?*

[10 marks/markah]

3. [a] The complex reactions  
*Tindak balas kompleks*



were carried out with pure A as feed.

*telah dijalankan dengan A tulen sebagai suapan.*

- [i] Derive an equation for A concentration as a function of time in a batch reactor. If  $k_1 = 0.01 \text{ s}^{-1}$ , what is the ratio of  $C_A/C_{A0}$  after 1.5 min?

*Terbitkan persamaan untuk kepekatan A sebagai fungsi masa dalam reaktor berkelompok. Jika  $k_1 = 0.01 \text{ s}^{-1}$ , apakah nisbah  $C_A/C_{A0}$  selepas 1.5 min?*

[5 marks/markah]

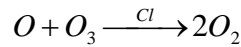
- [ii] If the series reaction is carried out in a continuous stirred reactor (CSTR), determine the reactor volume that will maximize the production of B for a volumetric flow rate of  $20 \text{ dm}^3/\text{min}$ . Please note that  $k_2 = 0.003 \text{ s}^{-1}$ ,  $k_3 = 0.002 \text{ s}^{-1}$  and  $C_{A0} = 0.2 \text{ g mol/dm}^3$ . (Hint:  $dC_B/dt = 0$ )

*Jika tindak balas bersiri ini dijalankan di dalam reaktor pengaduk berterusan, tentukan isipadu reaktor yang akan memaksimumkan pengeluaran B untuk kadar aliran isipadu sebanyak  $20 \text{ dm}^3/\text{min}$ . Sila ambil perhatian bahawa  $k_2 = 0.003 \text{ s}^{-1}$ ,  $k_3 = 0.002 \text{ s}^{-1}$  dan  $C_{A0} = 0.2 \text{ g mol/dm}^3$ . (Petunjuk:  $dC_B/dt = 0$ )*

[10 marks/markah]

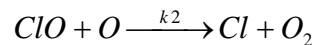
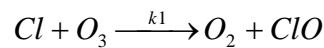
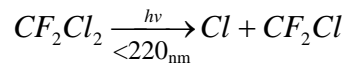
- [b] The decomposition of ozone can be accelerated in the presence of a catalyst such as chlorine atoms or radicals in the presence of fluorochlorocarbons.

*Penguraian ozon boleh dipercepatkan dalam kehadiran pemangkin seperti atom klorin atau radikal dalam kehadiran fluoroklorokarbon.*



The decomposition mechanisms are stated as below.

*Mekanisma penguraian dinyatakan seperti di bawah.*



Demonstrate that the decomposition rate is in the form of

*Tunjukkan bahawa kadar penguraian adalah dalam bentuk*

$$-r_{O_3} = k_2 C_{Cl}^T C_O$$

where  $C_{Cl}^T = C_{Cl} + C_{ClO}$  is constant

*di mana  $C_{Cl}^T = C_{Cl} + C_{ClO}$  adalah malar.*

[10 marks/markah]

4. [a] An elementary and irreversible reaction ( $A \rightarrow R$ ) occurs in a CSTR. The following information is given.

*Satu tindak balas asas dan tidak berbalik ( $A \rightarrow R$ ) berlaku di dalam reaktor pengaduk berterusan. Maklumat yang berikut diberikan.*

$$-r_A = e^{25} e^{-20000/RT} C_A \text{ (mol / L. min)}$$

$$C_{A0} = 1 \text{ mol / L}$$

$$T_0 = 350 \text{ K}$$

$$\Delta H_{RA} = -100,000 \text{ (cal / mol A)}$$

$$\rho C_p = 500 \text{ (cal / L. } ^\circ\text{C)}$$

- [i] Determine the reactor space time ( $\tau$ ) and heat to be removed for achieving 90 % of conversion at 350 K.

*Tentukan masa ruang reaktor ( $\tau$ ) dan haba yang perlu dibebaskan untuk mencapai 90% penukaran pada 350 K.*

[4 marks/markah]

- [ii] Determine the maximum adiabatic temperature and reactor space time ( $\tau$ ) needed for achieving 90% of conversion if the reaction is conducted adiabatically.

*Tentukan suhu maksimum adiabatik dan reaktor masa ruang ( $\tau$ ) yang diperlukan untuk mencapai 90% penukaran jika tindak balas dijalankan secara adiabatik.*

[6 marks/markah]

- [b] [i] Determine mean residence time ( $\bar{t}$ ) and plot the residence time distribution ( $E(t)$ ) from a cumulative distribution curve of a step response in Figure Q.4.[b].

*Tentukan purata masa mastautin ( $\bar{t}$ ) dan plotkan taburan masa mastautin ( $E(t)$ ) daripada lengkung taburan kumulatif bagi satu sambutan langkah dalam Rajah S.4.[b].*

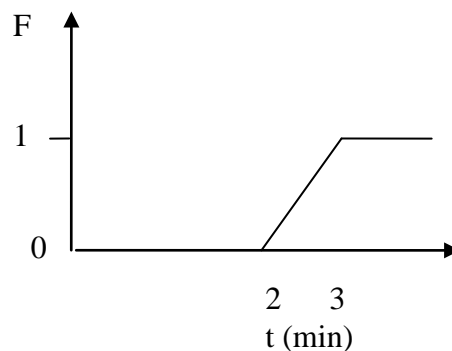


Figure Q.4.[b].

*Rajah S.4.[b].*

[5 marks/markah]

- [ii] An impulse tracer test produced the exit age distribution function presented in Table Q.4.[b]., for a reactor with a first-order reaction (rate constant  $k = 0.1 \text{ min}^{-1}$ ). Find the reactant conversion for two different assumptions which are ideal plug flow and perfect mixing. What do you expect on the real conversion?

*Satu ujian pengesan dedenyut menghasilkan fungsi taburan umur keluar yang dibentangkan dalam Jadual S.4.[b]., untuk satu reaktor dengan tindak balas tertib pertama (pemalar kadar  $k = 0.1 \text{ min}^{-1}$ ). Carikan penukaran bahan tindak balas untuk dua andaian yang berbeza, iaitu aliran palam yang ideal dan percampuran sempurna. Apa yang anda ramalkan pada penukaran sebenar?*

Table Q.4.[b].

*Jadual S.4.[b].*

t (min)	0	5	10	15	20	25	30	35	40
E(t) ( $\text{min}^{-1}$ )	0	0.030	0.050	0.050	0.040	0.020	0.010	0.002	0

[10 marks/markah]

## Appendix

# Numerical A Techniques

## A.1 Useful Integrals in Reactor Design

Also see <http://www.integrals.com>

$$\int_0^x \frac{dx}{1-x} = \ln \frac{1}{1-x} \quad (\text{A-1})$$

$$\int_0^x \frac{dx}{(1-x)^2} = \frac{x}{1-x} \quad (\text{A-2})$$

$$\int_0^x \frac{dx}{1+\varepsilon x} = \frac{1}{\varepsilon} \ln(1+\varepsilon x) \quad (\text{A-3})$$

$$\int_0^x \frac{1+\varepsilon x}{1-x} dx = (1+\varepsilon) \ln \frac{1}{1-x} - \varepsilon x \quad (\text{A-4})$$

$$\int_0^x \frac{1+\varepsilon x}{(1-x)^2} dx = \frac{(1-\varepsilon)x}{1-x} - \varepsilon \ln \frac{1}{1-x} \quad (\text{A-5})$$

$$\int_0^x \frac{(1+\varepsilon x)^2}{(1-x)^2} dx = 2\varepsilon(1+\varepsilon) \ln(1-x) + \varepsilon^2 x + \frac{(1+\varepsilon)^2 x}{1-x} \quad (\text{A-6})$$

$$\int_0^x \frac{dx}{(1-x)(\Theta_B - x)} = \frac{1}{\Theta_B - 1} \ln \frac{\Theta_B - x}{\Theta_B(1-x)} \quad \Theta_B \neq 1 \quad (\text{A-7})$$

$$\int_0^x \frac{dx}{ax^2 + bx + c} = \frac{-2}{2ax + b} + \frac{2}{b} \quad \text{for } b^2 = 4ac \quad (\text{A-8})$$

$$\int_0^x \frac{dx}{ax^2 + bx + c} = \frac{1}{a(p-q)} \ln \left( \frac{q}{p} \cdot \frac{x-p}{x-q} \right) \quad \text{for } b^2 > 4ac \quad (\text{A-9})$$

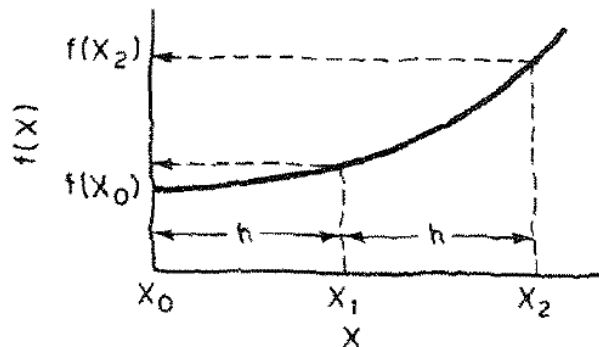
$$\int_0^W (1 - \alpha W)^{1/2} dW = \frac{2}{3\alpha} [1 - (1 - \alpha W)^{3/2}] \quad (\text{A-10})$$

*Simpson's one-third rule* (three-point) (Figure A-3). A more accurate evaluation of the integral can be found with the application of Simpson's rule:

$$\int_{X_0}^{X_2} f(X) dX = \frac{h}{3} [f(X_0) + 4f(X_1) + f(X_2)] \quad (\text{A-20})$$

where

$$h = \frac{X_2 - X_0}{2} \quad X_1 = X_0 + h$$



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**Figure A-3** Simpson's three-point rule illustration.

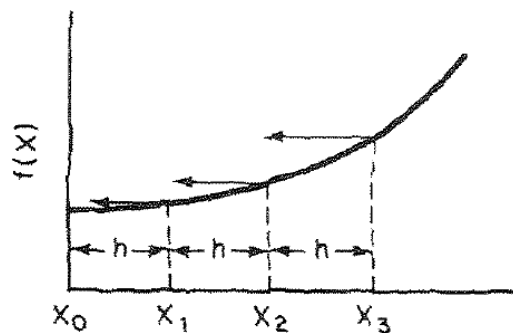
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*Simpson's three-eighths rule* (four-point) (Figure A-4). An improved version of Simpson's one-third rule can be made by applying *Simpson's second rule*:

$$\int_{X_0}^{X_3} f(X) dX = \frac{3}{8}h [f(X_0) + 3f(X_1) + 3f(X_2) + f(X_3)] \quad (\text{A-21})$$

where

$$h = \frac{X_3 - X_0}{3} \quad X_1 = X_0 + h \quad X_2 = X_0 + 2h$$



**Figure A-4** Simpson's four-point rule illustration.



***Ideal Gas Constant***

$$R = \frac{8.314 \text{ kPa} \cdot \text{dm}^3}{\text{mol} \cdot \text{K}}$$

$$R = \frac{1.987 \text{ Btu}}{\text{lb mol} \cdot ^\circ\text{R}}$$

$$R = \frac{0.73 \text{ ft}^3 \cdot \text{atm}}{\text{lb mol} \cdot ^\circ\text{R}}$$

$$R = \frac{8.3144 \text{ J}}{\text{mol} \cdot \text{K}}$$

$$R = 0.082 \frac{\text{dm}^3 \cdot \text{atm}}{\text{mol} \cdot \text{K}} = \frac{0.082 \text{ m}^3 \cdot \text{atm}}{\text{kmol} \cdot \text{K}}$$

$$R = \frac{1.987 \text{ cal}}{\text{mol} \cdot \text{K}}$$

***Temperature***

$$^\circ\text{F} = 1.8 \times ^\circ\text{C} + 32$$

$$\text{R} = ^\circ\text{F} + 459.69$$

$$\text{K} = ^\circ\text{C} + 273.16$$

$$^\circ\text{R} = 1.8 \times \text{K}$$

$$^\circ\text{Réamur} = 1.25 \times ^\circ\text{C}$$

First Point  $\left. \frac{dC_A}{dt} \right|_{t_0} = \frac{-3C_{A0} + 4C_{A1} - C_{A2}}{2\Delta t}$

Interior Points or Median  $\left. \frac{dC_A}{dt} \right|_{t_i} = \frac{C_{A(i+1)} - C_{A(i-1)}}{2\Delta t}$

Last Point or Third quartile  $\left. \frac{dC_A}{dt} \right|_{t_n} = \frac{C_{A(n-2)} - 4C_{A(n-1)} + 3C_{A(n)}}{2\Delta t}$

Useful differential equations:

$$\frac{d}{dx}(uv) = u \frac{dv}{dx} + v \frac{du}{dx}$$

$$\frac{d}{dx}(u/v) = \frac{(v \frac{du}{dx} - u \frac{dv}{dx})}{v^2}$$

## Numerical Evaluation of Integrals:

### 1. Trapezoidal rule

$$\int_{x_0}^{x_1} f(x)dx = \frac{h}{2}[f(x_0) + f(x_1)] \text{ when } h = x_1 - x_0$$

### 2. Simpson's three-eighths rule

$$\int_{x_0}^{x_3} f(x)dx = \frac{3}{8}h[f(x_0) + 3f(x_1) + 3f(x_2) + f(x_3)]$$

$$\text{Where } h = \frac{x_3 - x_0}{3}; \quad x_1 = x_0 + h; \quad x_2 = x_0 + 2h;$$

### 3. Simpson's quadrature formula

$$\int_{x_0}^{x_4} f(x)dx = \frac{h}{3}[f(x_0) + 4f(x_1) + 2f(x_2) + 4f(x_3) + f(x_4)]$$

$$\text{Where } h = \frac{x_4 - x_0}{4}$$

### 4. For N+1 points, where (N/3) is an integer,

$$\int_{x_0}^{x_N} f(x)dx = \frac{3}{8}h[f(x_0) + 3f(x_1) + 3f(x_2) + 2f(x_3) + 3f(x_4) + 3f(x_5) + \cdots + 3f(x_{N-1}) + f(x_N)]$$

$$\text{Where } h = \frac{x_N - x_0}{N}$$

### 5. For N+1 points, where N is even,

$$\int_{x_0}^{x_N} f(x)dx = \frac{h}{3}[f(x_0) + 4f(x_1) + 2f(x_2) + 4f(x_3) + 2f(x_4) + \cdots + 4f(x_{N-1}) + f(x_N)]$$

$$\text{Where } h = \frac{x_N - x_0}{N}$$

Ideal gas constant

$$R = \frac{8.314 \text{ kPa} \cdot \text{dm}^3}{\text{mol} \cdot \text{K}}$$

$$R = \frac{1.987 \text{ Btu}}{\text{lb mol} \cdot ^\circ \text{R}}$$

$$R = \frac{0.73 \text{ ft}^3 \cdot \text{atm}}{\text{lb mol} \cdot ^\circ \text{R}}$$

$$R = \frac{8.3144 \text{ J}}{\text{mol} \cdot \text{K}}$$

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$$R = \frac{1.987 \text{ cal}}{\text{mol} \cdot \text{K}}$$

**First Point**

$$\left. \frac{dC_A}{dt} \right|_{t_0} = \frac{-3C_{A0} + 4C_{A1} - C_{A2}}{2\Delta t}$$

**Interior Points**

$$\left. \frac{dC_A}{dt} \right|_{t_i} = \frac{C_{A(i+1)} - C_{A(i-1)}}{2\Delta t}$$

**Last point**

$$\left. \frac{dC_A}{dt} \right|_{t_n} = \frac{C_{A(n-2)} - 4C_{A(n-1)} + 3C_{A(n)}}{2\Delta t}$$

Energy balance:

$$T = T_0 + \frac{X[-\Delta H_{Rx}(T_0)]}{\sum \phi_i \tilde{C}_{Pi} + X\Delta \tilde{C}_P}$$

Rate law:

$$k(T) = k(T_1)e^{\left[ \frac{E}{R} \left( \frac{1}{T_1} - \frac{1}{T} \right) \right]}$$

## Useful Integrals in Reactor Design

$$\int_0^x \frac{dx}{1-x} = \ln \frac{1}{1-x} \quad (\text{A-1})$$

$$\int_0^x \frac{dx}{(1-x)^2} = \frac{x}{1-x} \quad (\text{A-2})$$

$$\int_0^x \frac{dx}{1+\varepsilon x} = \frac{1}{\varepsilon} \ln(1+\varepsilon x) \quad (\text{A-3})$$

$$\int_0^x \frac{1+\varepsilon x}{1-x} dx = (1+\varepsilon) \ln \frac{1}{1-x} - \varepsilon x \quad (\text{A-4})$$

$$\int_0^x \frac{1+\varepsilon x}{(1-x)^2} dx = \frac{(1-\varepsilon)x}{1-x} - \varepsilon \ln \frac{1}{1-x} \quad (\text{A-5})$$

$$\int_0^x \frac{(1+\varepsilon x)^2}{(1-x)^2} dx = 2\varepsilon(1+\varepsilon) \ln(1-x) + \varepsilon^2 x + \frac{(1+\varepsilon)^2 x}{1-x} \quad (\text{A-6})$$

$$\int_0^x \frac{dx}{(1-x)(\Theta_B - x)} = \frac{1}{\Theta_B - 1} \ln \frac{\Theta_B - x}{\Theta_B (1-x)} \quad \Theta_B \neq 1 \quad (\text{A-7})$$

$$\int_0^x \frac{dx}{ax^2 + bx + c} = \frac{-2}{2ax + b} + \frac{2}{b} \quad \text{for } b^2 = 4ac \quad (\text{A-8})$$

$$\int_0^x \frac{dx}{ax^2 + bx + c} = \frac{1}{a(p-q)} \ln \left( \frac{q}{p} \cdot \frac{x-p}{x-q} \right) \quad \text{for } b^2 > 4ac \quad (\text{A-9})$$

$$\int_0^W (1-\alpha W)^{1/2} dW = \frac{2}{3\alpha} \left[ 1 - (1-\alpha W)^{3/2} \right] \quad (\text{A-10})$$

$$\int_0^\infty (e^{-kt}) \delta(t-\tau) dt = e^{-k\tau} \quad (\text{A-11})$$

## Simpson's five-point formula

$$\int_{x_0}^{x_4} f(x) dx = \frac{h}{3} (f_0 + 4f_1 + 2f_2 + 4f_3 + f_4) \quad h = \frac{X_4 - X_0}{4}$$